



Going Beyond Rigid Aeroshells:

"Enabling Venus and Outer-Planet In-Situ Science Missions with Deployables"
Entry Systems & Technology Division

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- ◆ Portions of work conducted under NASA Ames contract NNA10DE12C to ERC, Inc
- ◆ Discussion with Dr. Lori Glaze, Dr. Jim Garvin and Mr. Charles Baker of NASA Goddard Space Flight Center and Peter Gage of Neerim Corporation is greatly appreciated
- ◆ Deployable Concept development (ADEPT) involved a large group across NASA Ames, Neerim Corp (Peter Gage), R.P.I. (Prof. Hajela) and Andrews Space (Dana Andrews)
- ◆ ADEPT relevant TPS testing was supported by JSC Arc jet group and BRM

Objective of this presentation:

- ◆ Venus and Outer-Planets (Saturn, Neptune, Uranus) in-situ science explorations are challenging. Part of the challenge is imposed by rigid aeroshell technology.
- ◆ Deployable or low ballistic coefficient aeroshell technology is a game changer
 - Very benign entry environment much more enabling of science
- ◆ Planned investments by Office of the Chief Technologist, has the potential to change the way we do EDL at Venus, Saturn, Neptune, Uranus, and Mars

Outline:

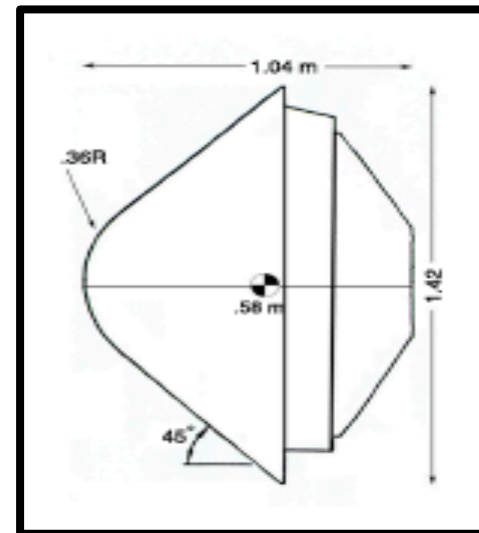
- ◆ High Ballistic Co-efficient (rigid) Aero-shell Technology (HBCAT)
- ◆ Entry at Venus, Saturn and Uranus using Low Ballistic Coefficient Aeroshell Technology (LBCAT)
- ◆ ADEPT and Flexible TPS Concepts Under Development
- ◆ Concluding Remarks
- ◆ Questions?

◆ P-V Probes: One Large Probe and three identical Small Probes

- Survival was a bonus.
- All but one survived impact, but all probes survived entry
- Entry Velocity 11.5 km/s

◆ Large Probe

- Ballistic Coefficient: 188 kg/m²; Size 1.42 m
- Entry Flight Path Angle: -32.4 deg at 200 km
- Peak heat-flux: 4500 W/cm² (~50% radiative)
- Total heat-load (stag): 12.4 KJ/cm²
- Peak stagnation pressure: ~10 atm.
- Probe Mass: 316.5 kg
- Peak deceleration: ~300g
- Mass Fraction of Carbon Phenolic TPS: 8.83%



Our Vision to Explore Venus: Mission Studies:



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	Mission	Date	Proposal
1	Venus Flagship Study (JPL Led)	2009	Flagship Study
2	ViTAL: Venus Intrepid Tessera Lander	2010	Decadal Study
3	VCM: Venus Climate Mission	2010	Decadal Study
4	VME: Venus Mobile Explorer	2010	Decadal Study

- **All the missions proposed use scaled P-V shape (45 deg sphere-cone)**
- **Rigid aeroshell with ballistic coefficient $\sim 200 \text{ kg/m}^2$**
- **Carbon Phenolic is the only viable TPS**
- **Large G'load during entry**

VME (2010) : A Flagship Class Mission Study Sponsored by Decadal Survey Committee



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Entry Velocity 11.3 km/s; EFPA – 21 deg
Aeroshell Size : 3.5 dia.
Entry Mass: 2921 Aeroshell Mass=1139 kg
Mass fraction of Aeroshell = 40%

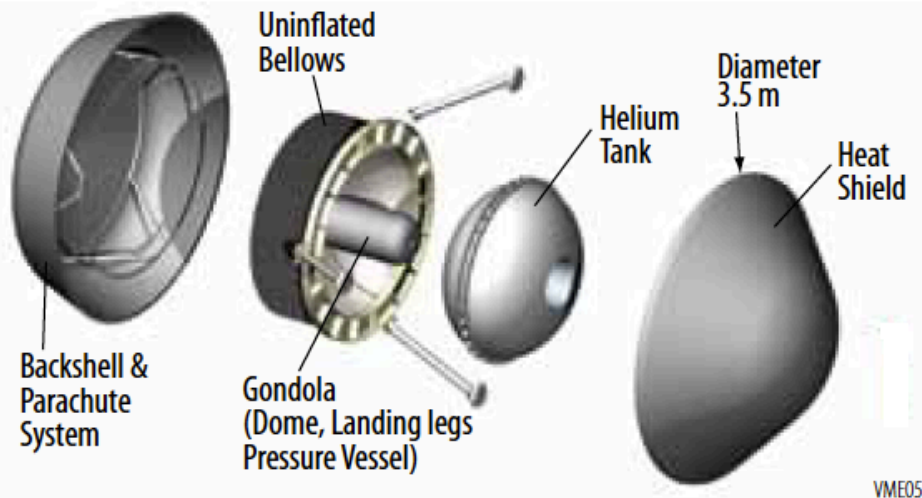


Figure 6: Aeroshell back shell and heat shield are based on Pioneer Venus Large Probe and Stardust geometries.

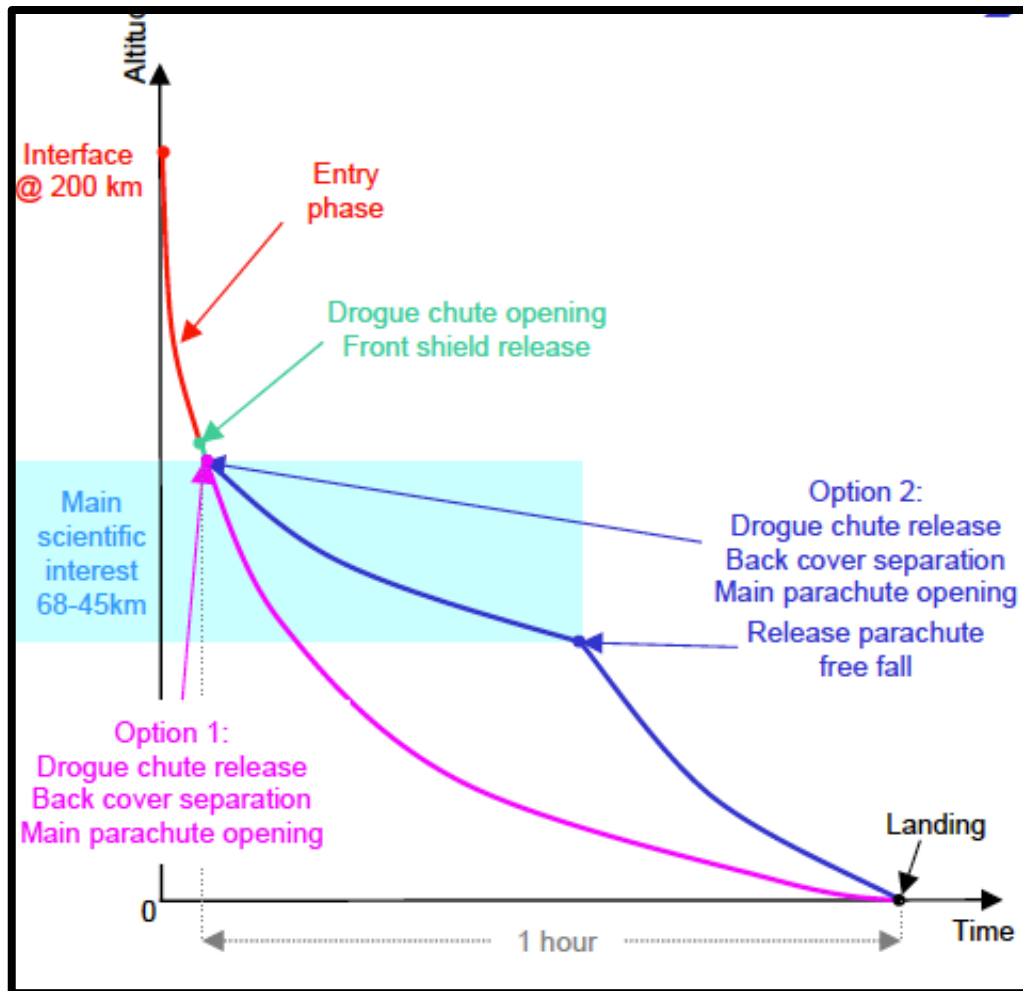
Table 9: Mission level mass rackup (Table 6 shows carrier details).

Item	CBE (kg)	Composite Mass Growth Allow. (%)	Max Expected Mass (kg)
Lander	1390	30%	1782
Lander Science Payload	31	30%	41
Lander Subsystems	469	30%	609
Mechanical/ Structure	270	30%	351
Mechanisms	51	30%	66
Thermal	113	30%	147
Other	34	30%	44
Bellows	890	30%	1132
Aeroshell	876	30%	1139
Spacecraft	846	30%	1100
Satellite (S/C + Probe) Dry Mass	3112	30%	4021
Propellant Mass	366	1%	370
Satellite Wet Mass	3478		4390
LV Throw Mass available to lift Wet			5141

Selecting EFPA and Ballistic Coefficient: Challenges to consider & Constraints that impacts Science Payload Mass



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Venus Entry and Descent Constraints:

- Max heat-flux
- Max total pressure
- Total heat load
- Max deceleration
- Max dynamic pressure vs alt.
- Drogue chute opening alt.
- Shield separation assurance
- Sizing main parachute for max descent time (toxic env.)
- Free fall time from 45km to surface (thermal problems)

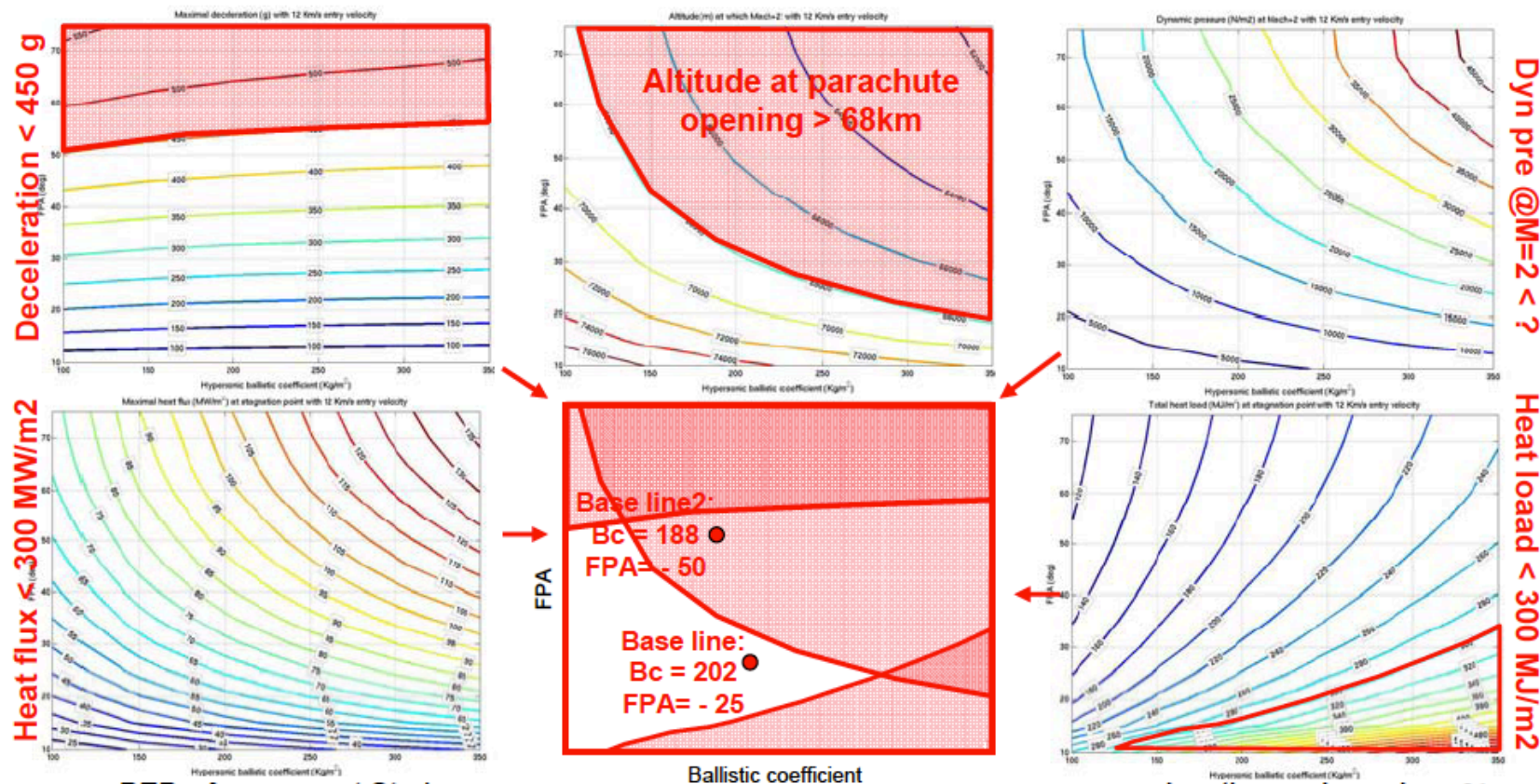
Acknowledgement: From ESA PEP Study Presentation

Selecting Entry Flight Path Angle and Ballistic Coefficient



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Venus: feasible domain @ 12 KM/s entry

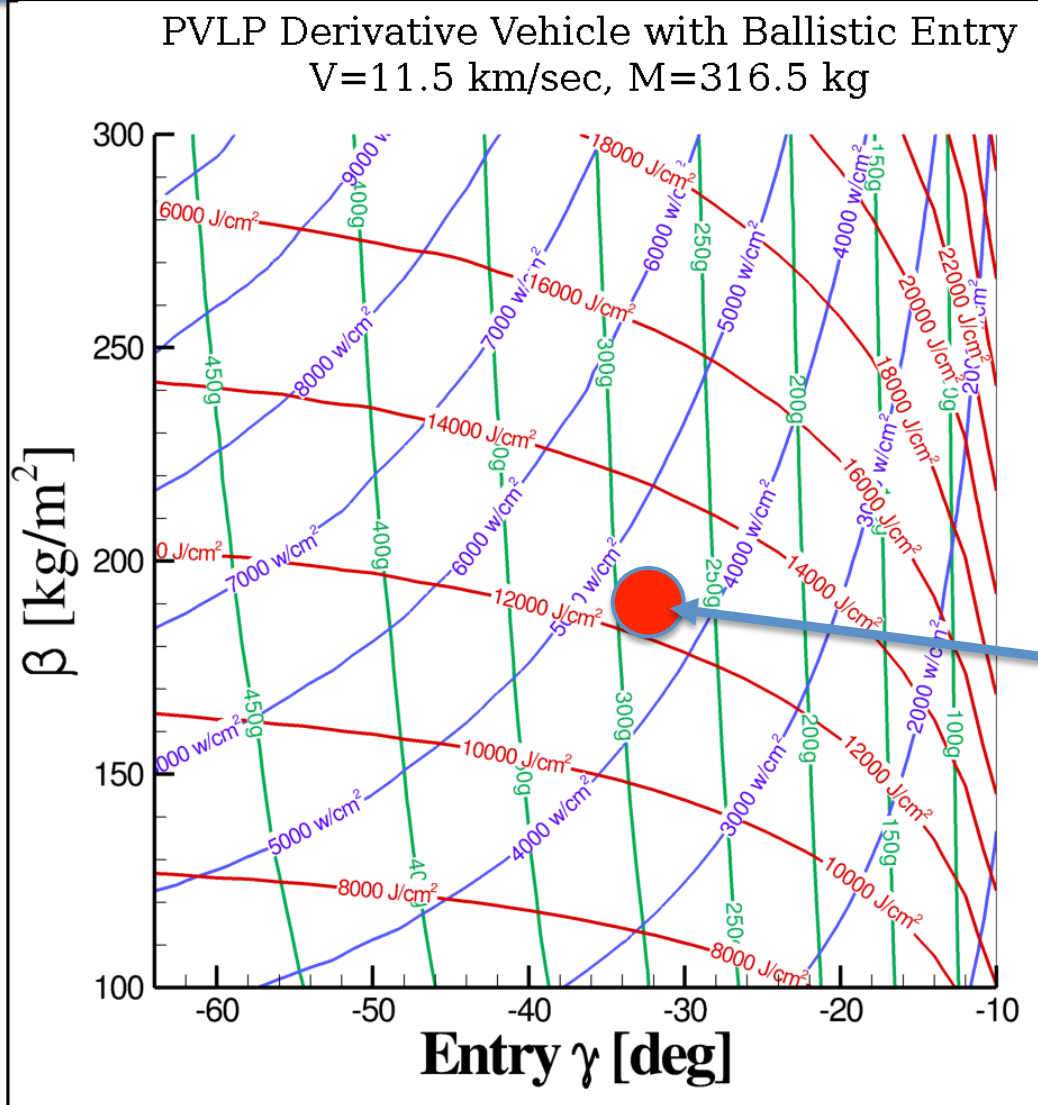


Acknowledgement: 2010 ESA Planetary Entry Probe (PEP) Assessment Study

A Carpet plot of Missions to Venus: High Ballistic Coefficient (P-V Probe Scaled)

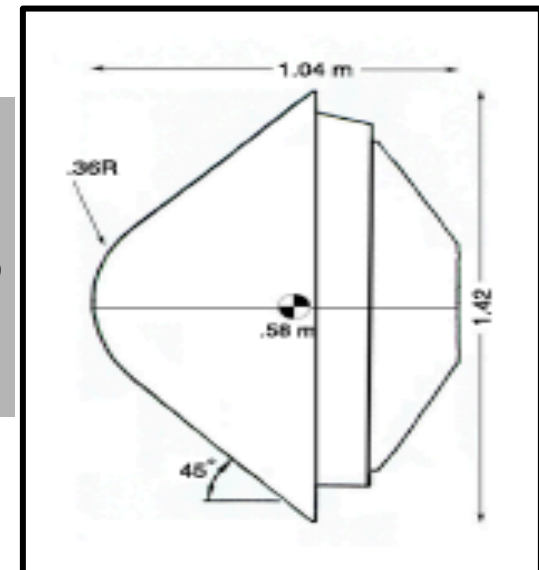


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- ◆ Skip-out is $\sim (-7.5^\circ)$
- ◆ Rigid Aeroshell Ballistic Coefficient (200 – 350)
- ◆ Entry Flight Path Angle
 - Lower EFP = Increased (heat-load and TPS Mass fraction)
 - Lower Ballistic Coefficient = lower payload mass

P-V Large Probe



Venus In-situ Missions: High Ballistic Coefficient Rigid Aeroshell Technology (HBCAT) Challenges



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High Ballistic Coefficient ~ 200 or higher

- For Heat-flux (2000 – 7000) w/cm² stag. pressure (2 – 10) atm, **Carbon phenolic** is the only choice
- Challenges for Carbon Phenolic are:
 - ◆ Especially need alternate to heritage, fully dense, chop-molded, Carbon Phenolic.
 - ◆ Lack of ground test facilities capabilities
 - Certification of Vendors and processes
 - TPS qualification, and flight heat shield certification
- High G'load during entry (200 g' – 450 g')
 - ◆ Robustness to high G' conditions adds mass and verification is a challenge
- 45 deg sphere-cone rigid aeroshell geometry
 - ◆ Packaging and C.G. constraints

LOW BALLISTIC COEFFICIENT AEROSHELL TECHNOLOGY (LBCAT)

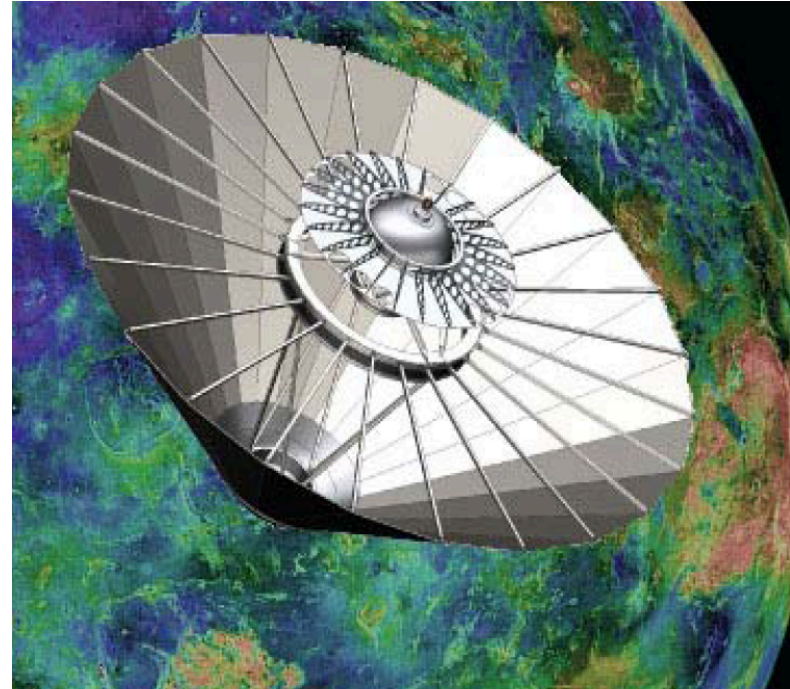


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Inflatable



**Mechanically
Deployable**



**If we can fly low ballistic coefficient aeroshell
at Venus, what would that buy?**


HBCAT and LBCAT



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Lowering β

- lower heat-flux
- lower heat-load
- Low entry mass or increased size



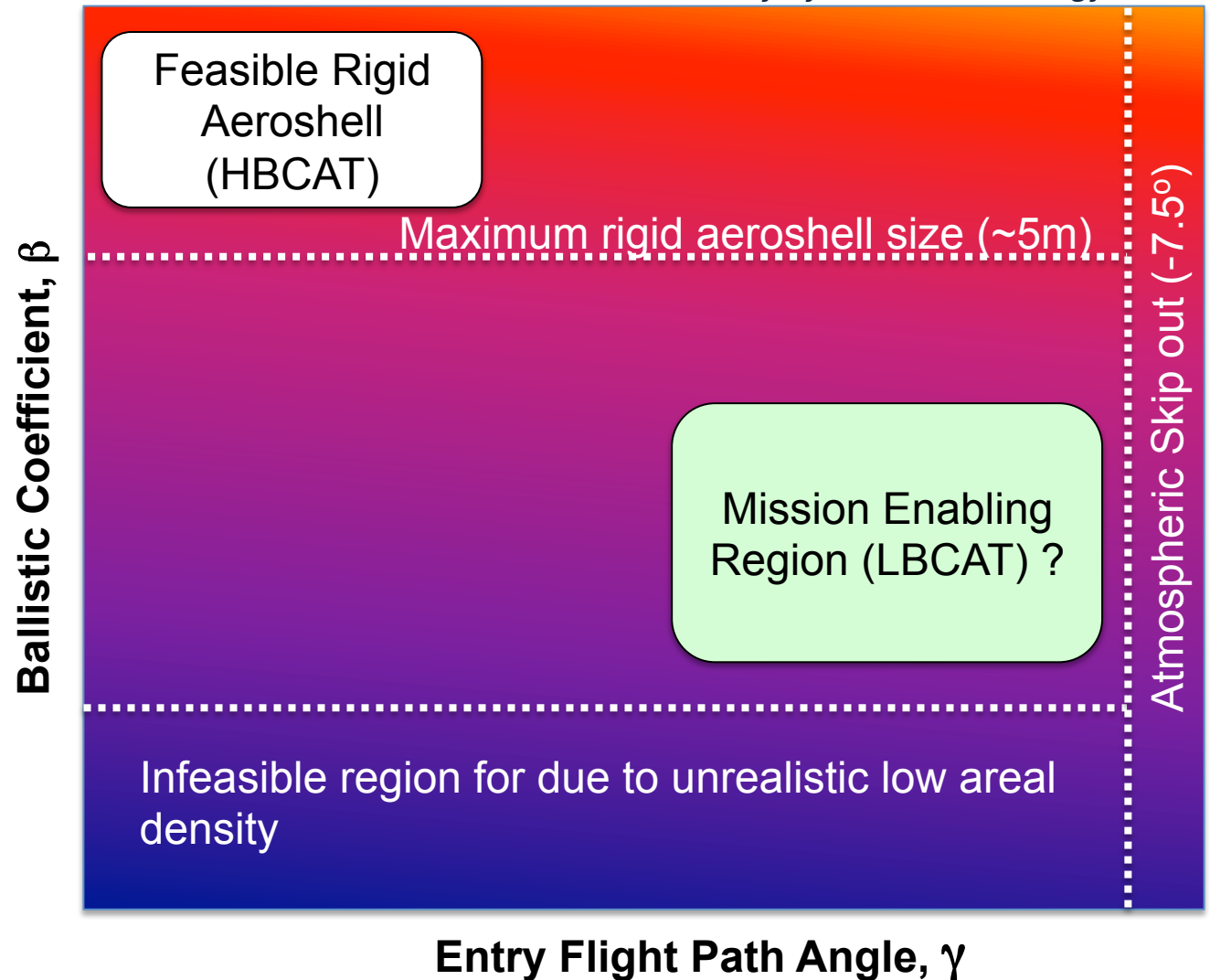

Lowering γ

- lower g'load
- raises heat-load
- raises heat-flux



Best is:

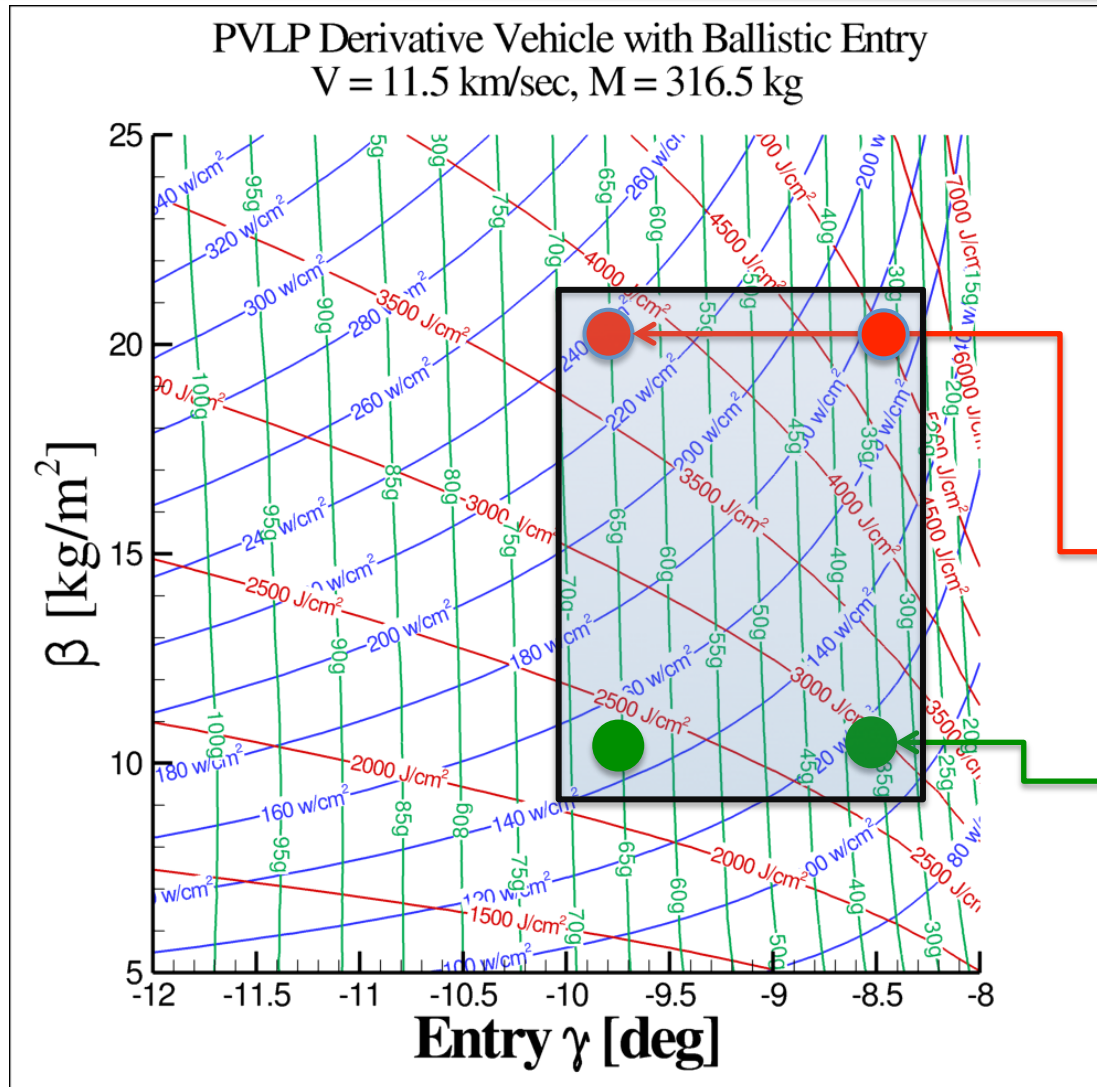
Lower β and γ together sufficiently so that entry mass is not increased significantly



Low Ballistic Coefficient Design Space: (P-V Probe Scaled)



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◆ Low (Ballistic Coefficient & EFPA)

- Low peak heat flux
- Low G'load
- Low heat load

**B=20 => P-V Large
Probe scaled to 4.0 m**

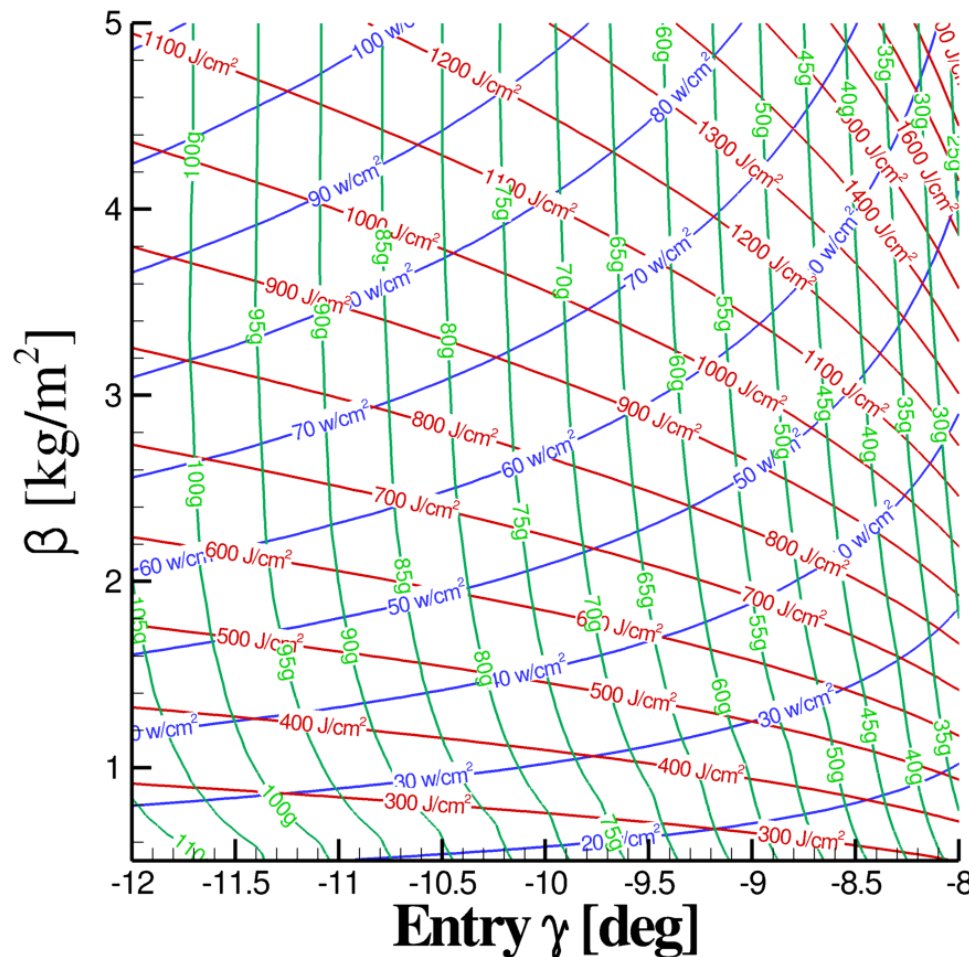
**B=10 => P-V Large
Probe scaled to 6.2 m**

What Happens With Even Lower Ballistic Coefficient in the Design Space?



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PVLP Derivative Vehicle with Ballistic Entry
 $V = 11.5 \text{ km/sec}$, $M = 316.5 \text{ kg}$



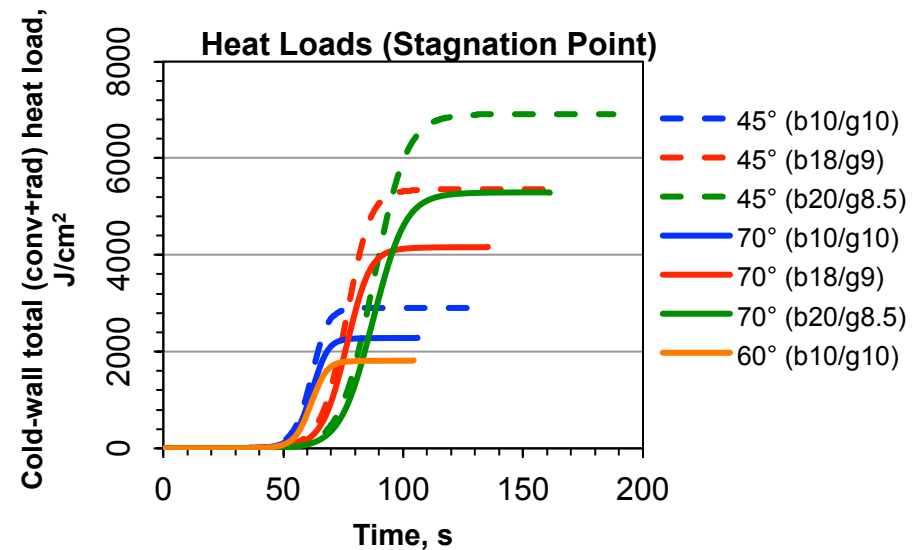
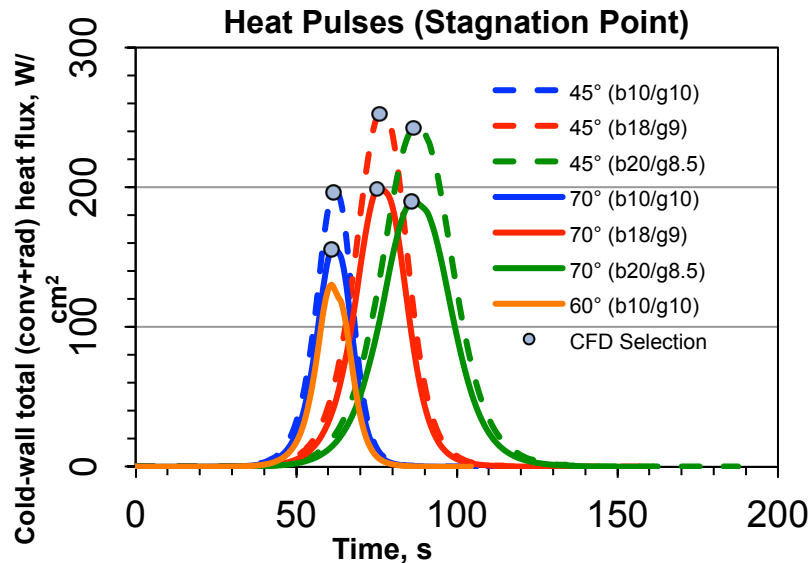
Lower β means

- Lower heat-flux and heat-load
- At β of 5 (dia. = $\sim 8.5\text{m}$) heat flux (60 – 110 W/cm^2)
- At β of 1 (dia. = $\sim 20 \text{ m}$) heat flux (25 – 35 W/cm^2)
- If the desire is to stay at very low heat-flux ($\sim 30 \text{ W/cm}^2$) and have some margin on γ , g-load starts to go back up
- Lower β (< 2) \Rightarrow very larger diameter/surface area and higher g-load

LBCAT – Venus - Parametric Study: Stagnation Point Peak Conditions



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- Ballistic Coefficient (10 – 30); Entry Mass (300 kg and 3000 kg); EFPA (-8.5, -9 and -10.0); Shapes Considered (70°, 60°, 45°)

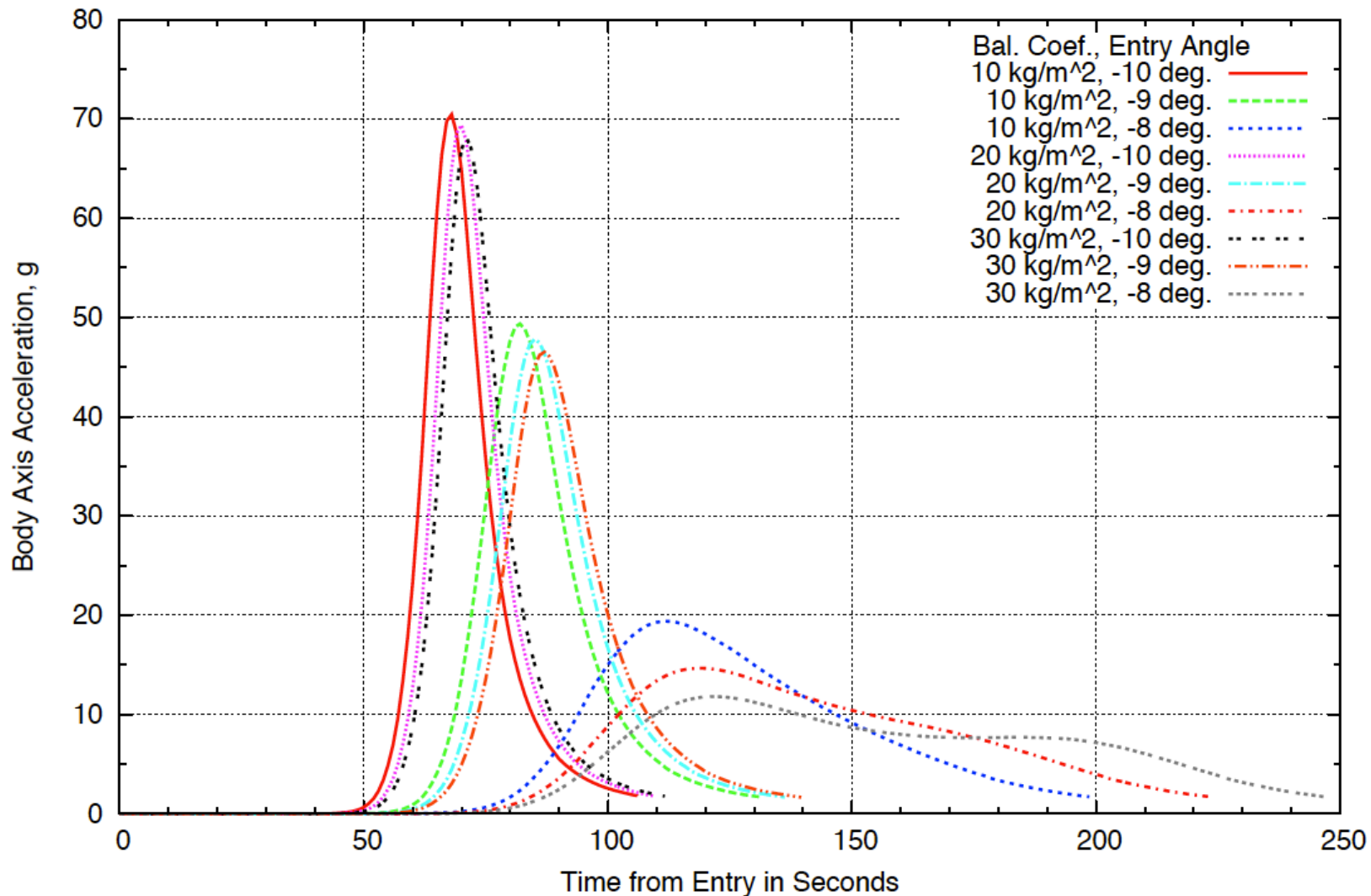
Observations:

- Low EFPA = Low G'load
- Low Ballistic Coeff. = Low heat load
- Stag. Heat-flux or Pressure not very sensitive
- Shape: 60 or 70 deg is more preferable than 45 deg sphere cones
- Heat load is sensitive

LBCAT for Venus EDL: Deceleration Profile During Entry (Entry Mass = 2000 kg; 70 deg. Sphere-Cone)



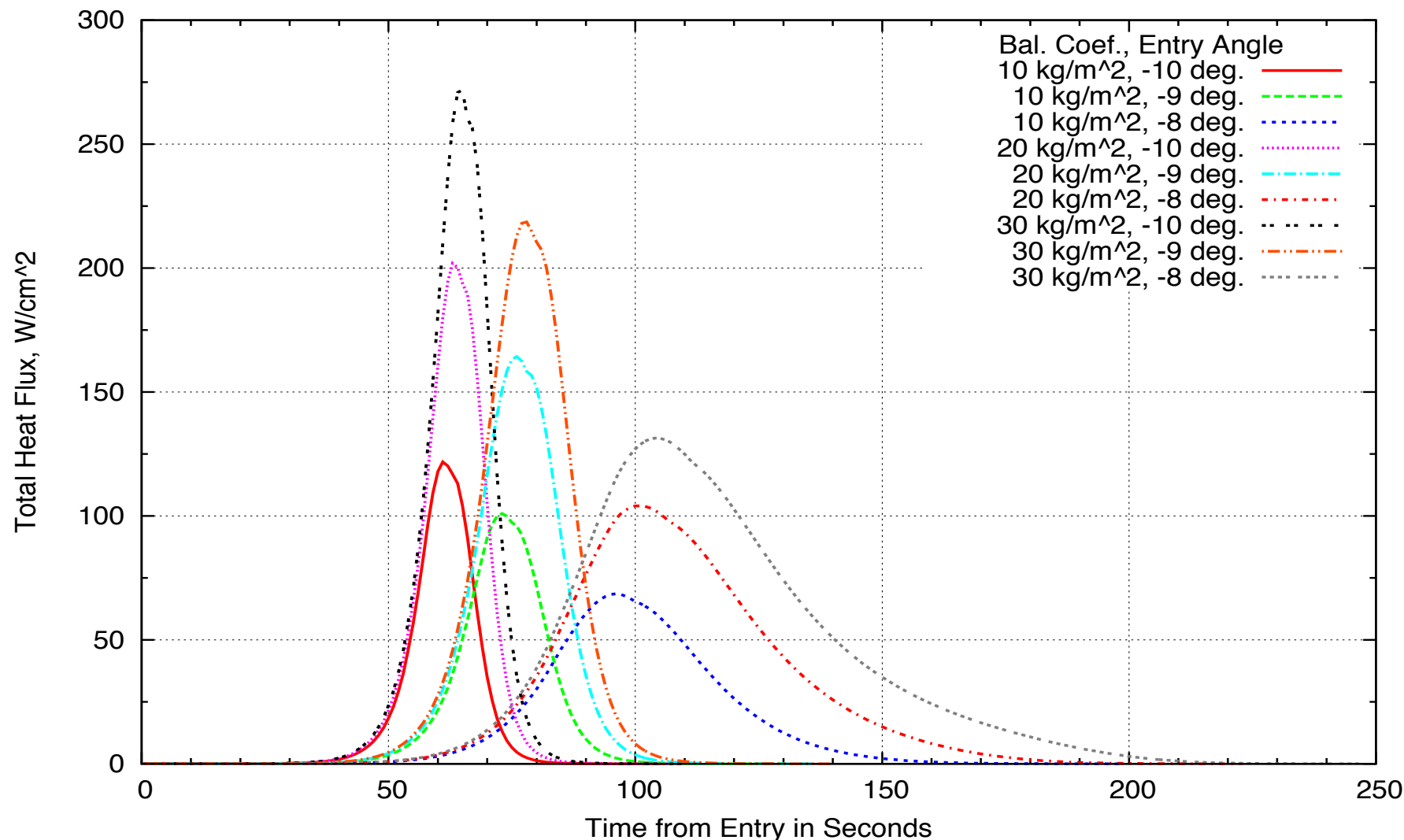
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LBCAT for Venus EDL: Stag. Point Total Heat-Flux During Entry (2000 kg Entry Mass and 70° Sph.-Cone)



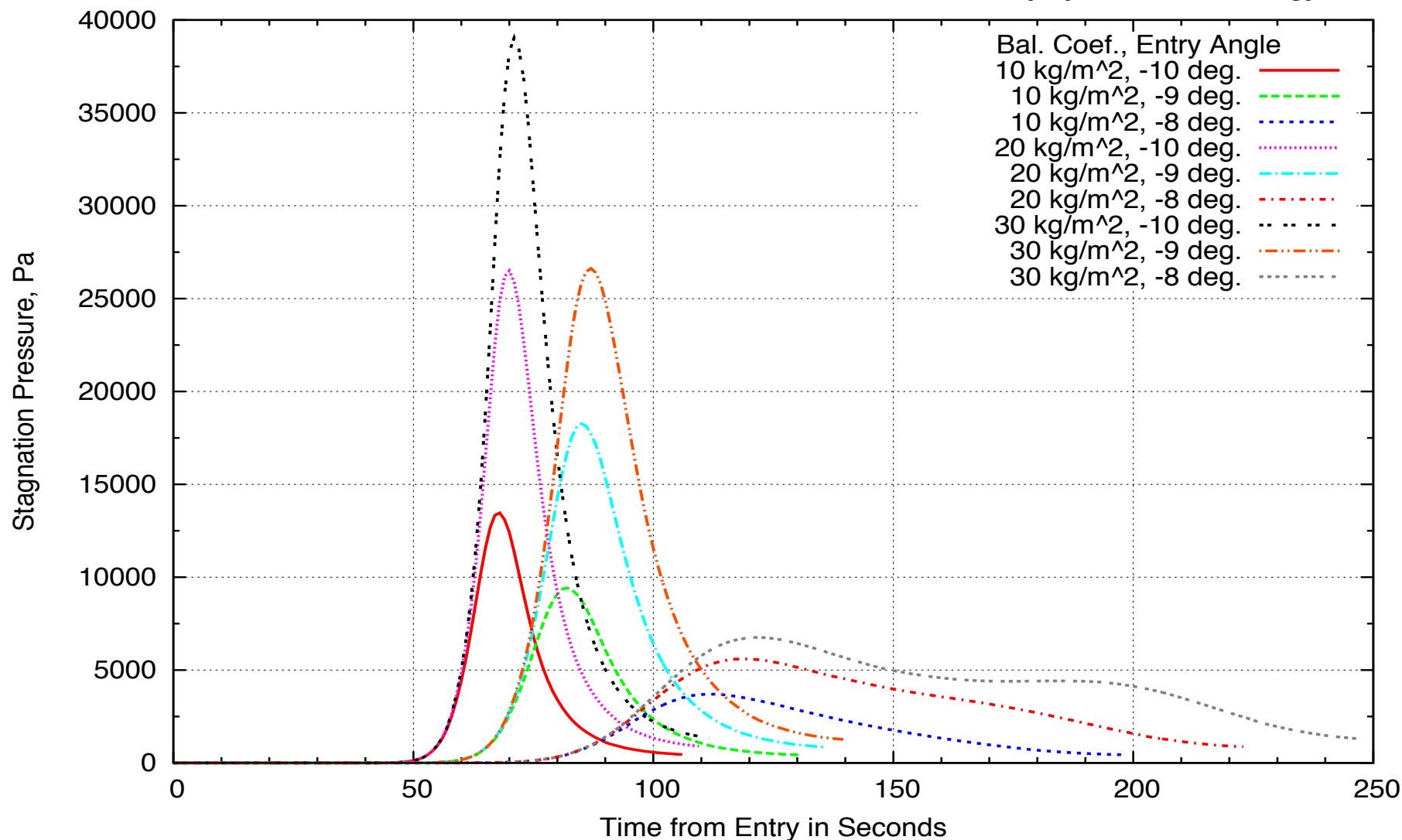
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LBCAT for Venus EDL: Stag. Pressure During Entry (2000 kg Entry Mass and 70° Sph.-Cone)



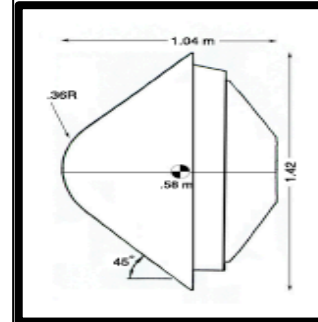
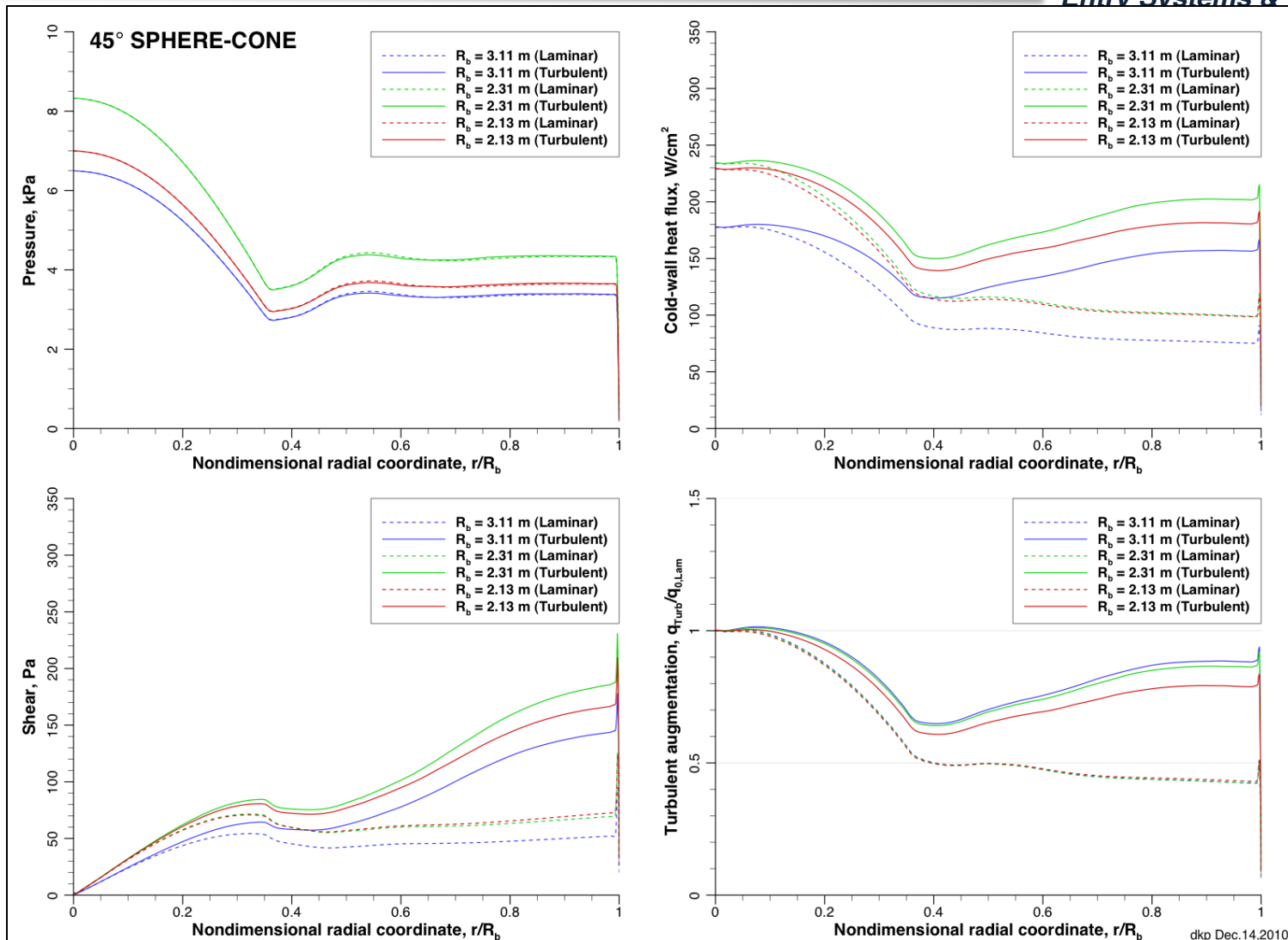
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Laminar vs Turbulent Heating at Peak Heat Flux Point Along the Trajectory (45 deg sphere cone Scaled P-V)



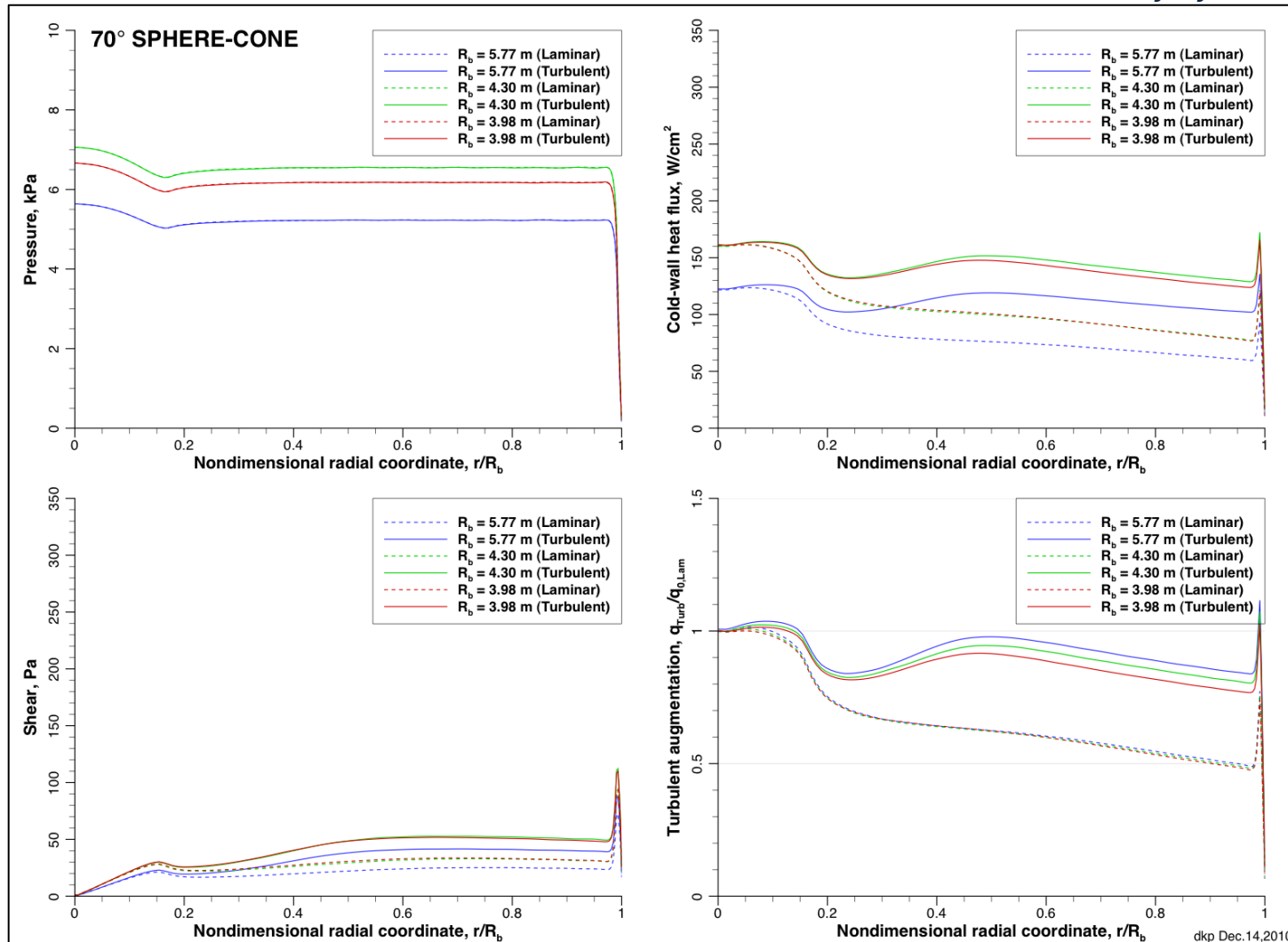
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Laminar vs Turbulent Heating at Peak Heating Point Along the Trajectory (70 deg sphere cone Scaled Viking)



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What about other Planets?

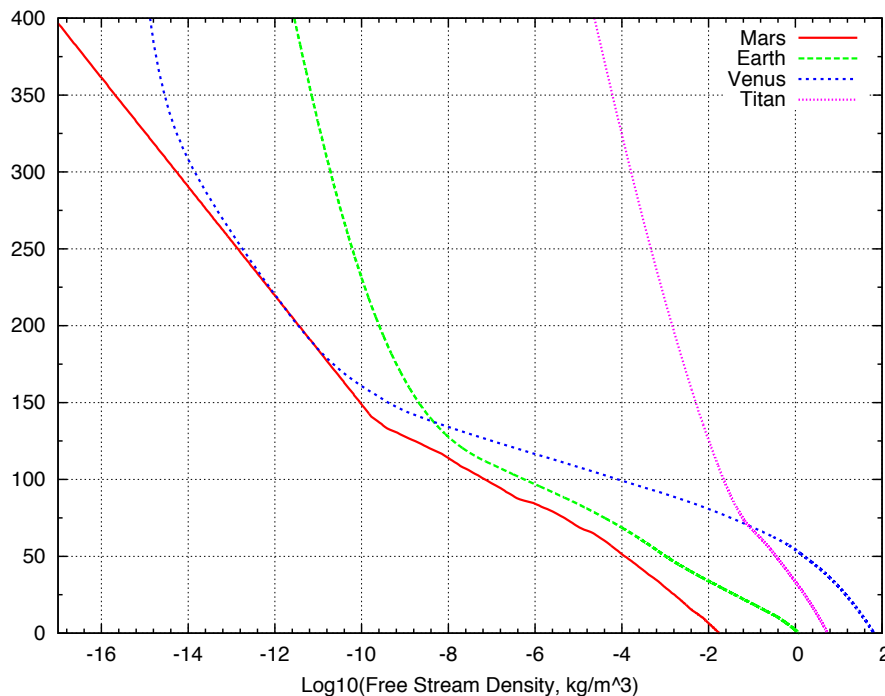


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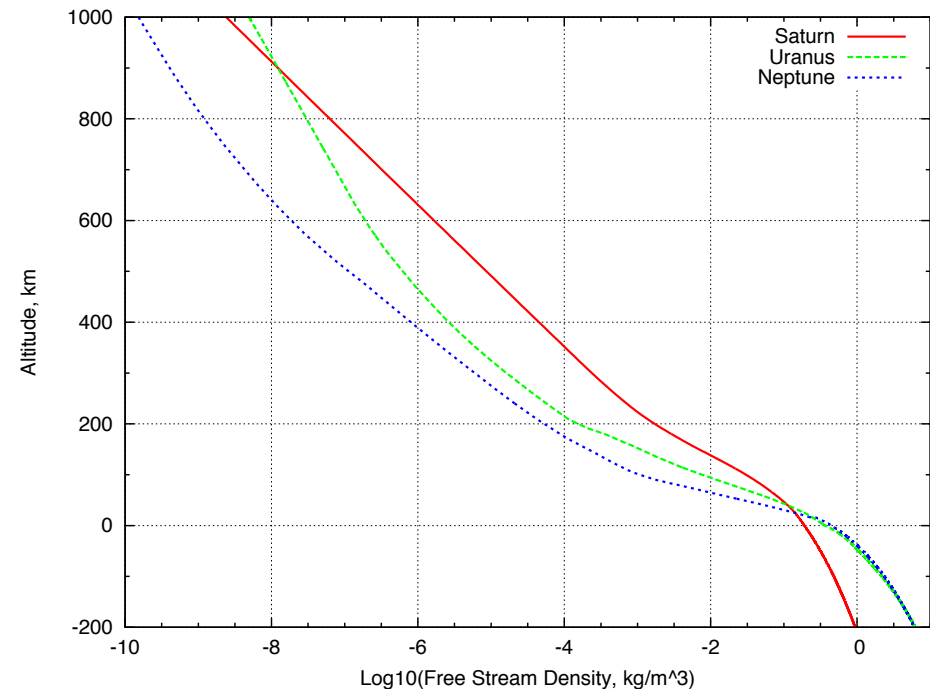
◆ Current Missions Studies for Saturn, Neptune and Uranus Probes use rigid aeroshell with high ballistic coefficient

- Face similar challenges as Venus
- High G'load, and high heat-flux and pressure needing Carbon Phenolic

Comparison of Atmospheric Density for Terrestrial Worlds

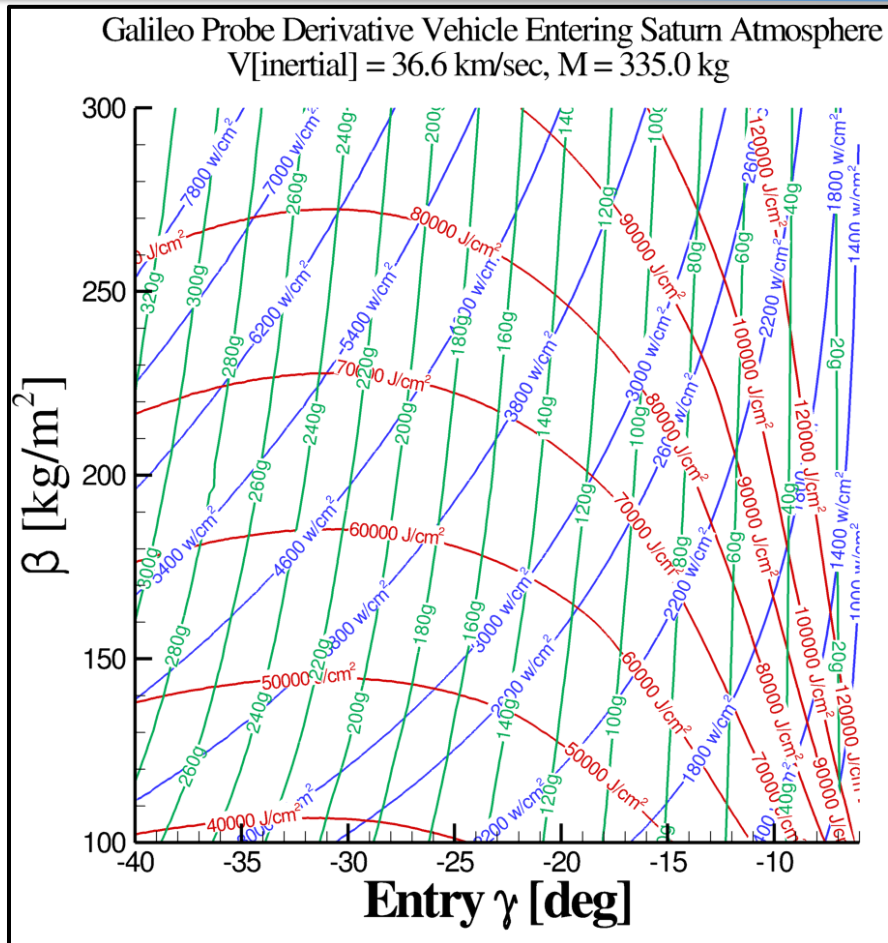


Comparison of Atmospheric Density for Giant Planets



LBCAT for Saturn:

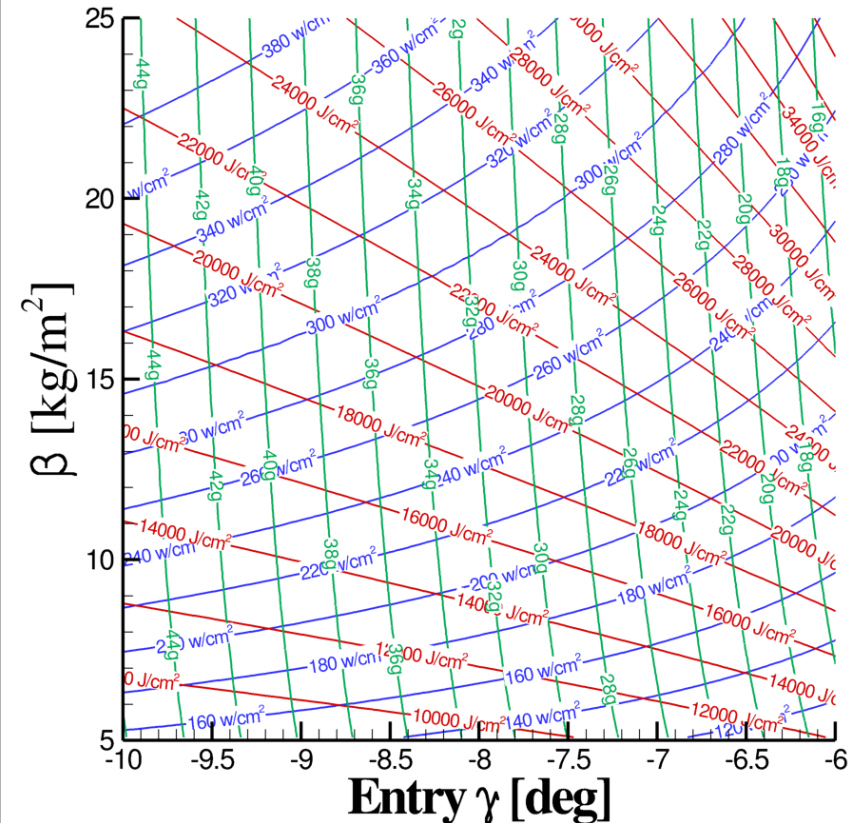
High Ballistic Coefficient Range



Low Ballistic Coefficient Range

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Galileo Probe Derivative Vehicle Entering Saturn Atmosphere
 $V[\text{inertial}] = 36.6 \text{ km/sec}$, $M = 335.0 \text{ kg}$



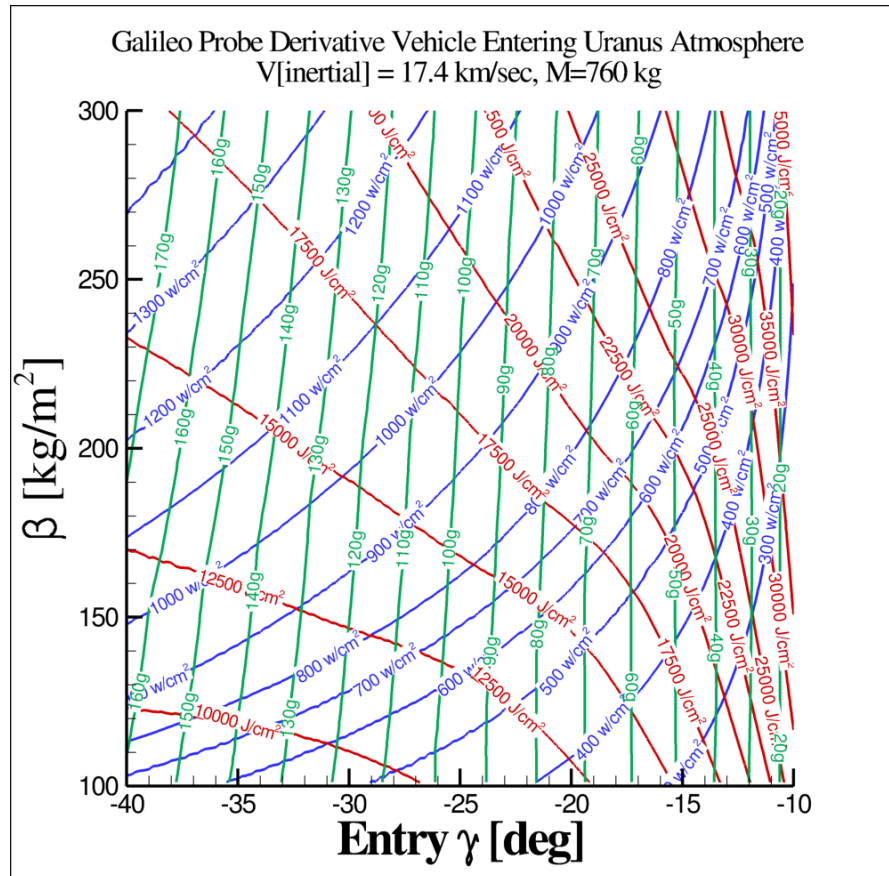
- LBCAT is as effective at Saturn as well (much reduced entry env.)
- Entry conditions are similar to Venus with LBCAT

LBCAT for Uranus:

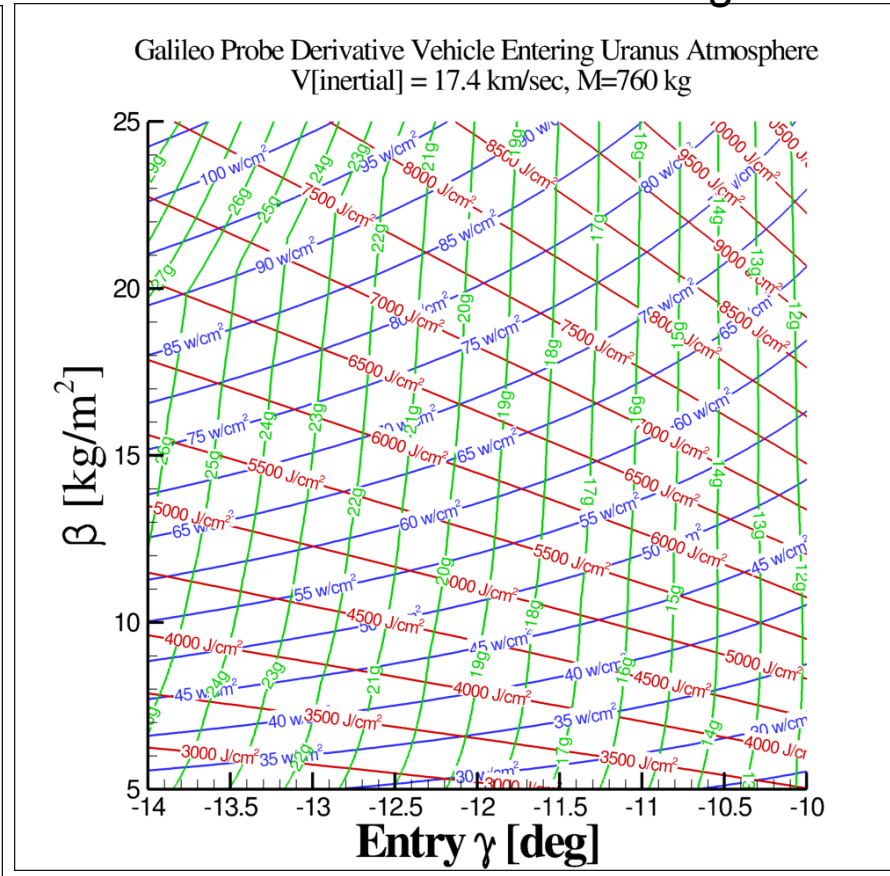


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High Ballistic Coefficient Range



Low Ballistic Coefficient Range



- LBCAT is as effective at Uranus as well (much reduced entry env.)
- Entry conditions are similar to Venus and Saturn

Summary: LBCAT for Venus, Saturn and Uranus (& most likely Neptune)



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◆ Low Ballistic Coefficient Technology

- Results in very benign Entry Conditions
 - Low heat-flux
 - Low pressure
 - Low heat load
 - Low G'load
- Challenges of testing and certification for flight is well within current facility capabilities
- Should result in lower Risk and Cost

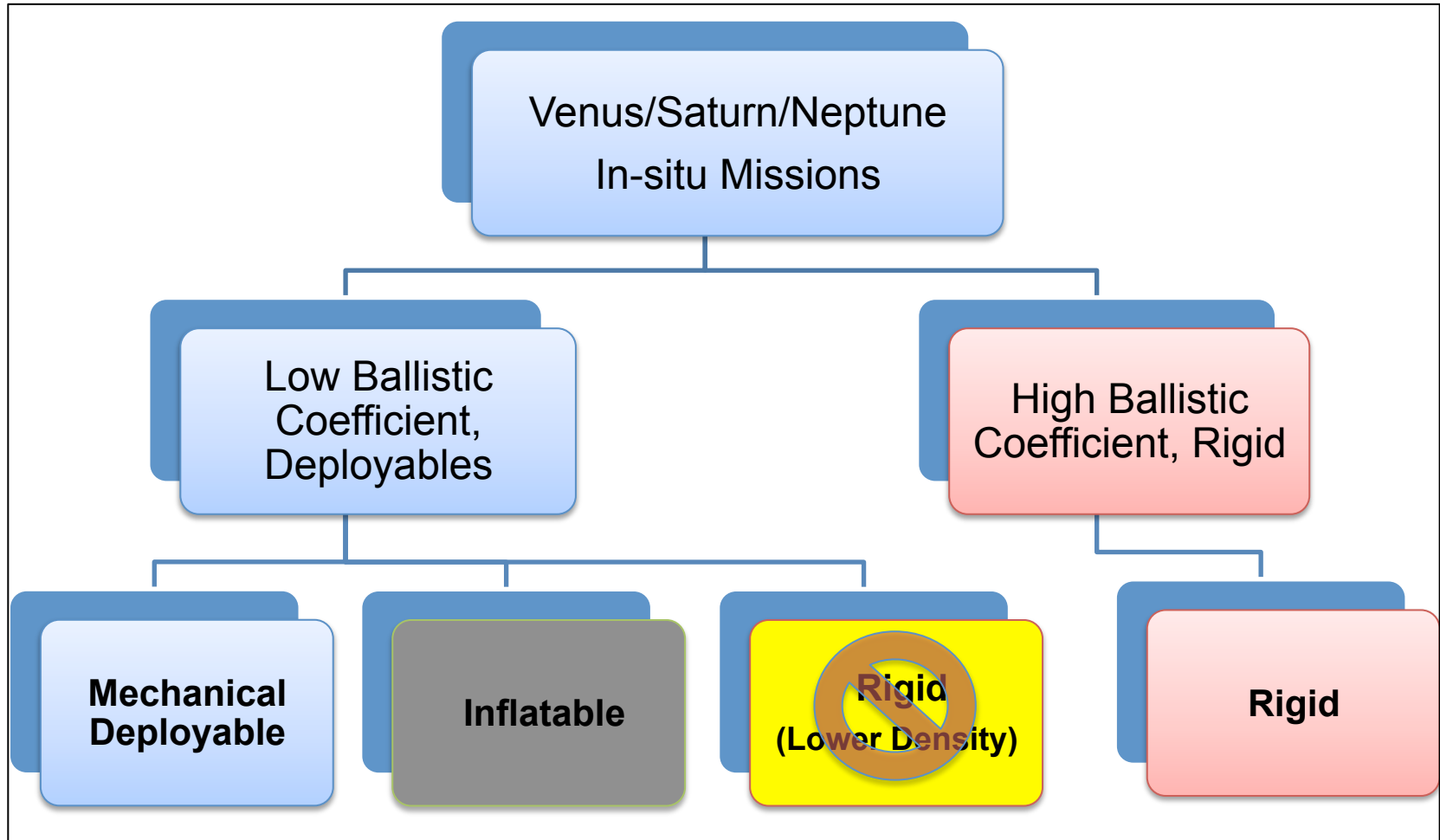
◆ Science Enabler

- Allows for inclusion of sensitive instrumentation
- Integration and certification is much easier
- More attractive for integrating ASRG technology

How can we achieve LBCAT?



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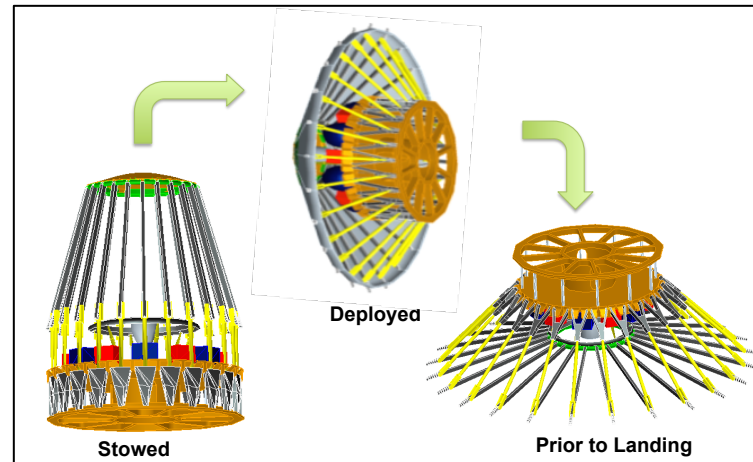
Deployable Entry System Concepts



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◆ Adaptable, Deployable Entry and Placement Technology (ADEPT)

- Concept study proposed under IPP and completed in Nov 2010



- ◆ Our motivation for exploring Venus, Saturn and Uranus is that it will be a stepping stone for Technologies such as ADEPT and Flexible TPS
- ◆ OCT is investing in both ADEPT as well as HIAD and the investment will mature these technologies to TRL 5-6 in 3 years.
- ◆ On going HIAD design at present is looking at inflatable systems with relatively low heat-flux capabilities ($< 50 \text{ W/cm}^2$)
- ◆ ADPET is looking at high heat-flux ($\sim 250 \text{ W/cm}^2$) capable entry systems

Flexible, High Heat-flux, Ablative TPS Development:



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- ◆ **OCT Game Changing Technologies Division is investing in Flexible, Ablative TPS starting (2012 – 2014) leveraging the investment made by ARMD and ESMD mission directorates in the past few years**
 - **3 year project to result in TRL 5-6**
 - **High heat flux ($> 250 \text{ W/cm}^2$)**
 - **System integration with inflatable or mechanically deployable (ADEPT)**

Concluding Remarks



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- ◆ **Use of rigid aeroshell (high ballistic coefficient) challenges, though limiting, helped achieve great science in the past**
 - Pioneer-Venus and Galileo
- ◆ **Current manufacturing (Carbon-Phenolic) and test facility (arc jet) limitations as well as more demanding mission requirements (value proposition) needs**
 - Alternate architectures and technologies has the potential to make Venus and OP missions less risky and more cost effective
 - This does not mean we are giving up or advocating against Carbon Phenolic
- ◆ **OCT is investing in low ballistic coefficient deployable technologies, such as semi-rigid and inflatable, as well as flexible high heat-flux TPS**
- ◆ **Successfully maturing these technologies will have “game-changing” impact and enable better science missions**

1. “Adaptive Deployable Entry and Placement Technology (ADEPT):A Feasibility Study for Human Missions to Mars,” E.Venkatapathy, et.al., AIAA Paper #2011-2608, 21st AIAA Aerodynamic Decelerator Systems Technology Conference and Seminar, Dublin, Ireland, 23-26 May 2011